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RADC-TR-84-148 In-House Report June 1984



LUMPED CIRCUIT TRANSMISSION LINE MODEL

Douglas H. Coivin

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#### Lumped Circuit Transmission Line Model

#### INTRODUCTION

Several computer aided design (CAD) programs require lumped circuit component values (resistors, inductors, and capacitors) as input data. It is often difficult, if not impossible, for a user of these CAD programs to mix distributed and lumped circuit parameters. Lumped circuit equivalents of distributed circuits are desired for sake of compatibility.

Transmission line responses are governed by distributed parameters. In this report, the development of a lumped circuit model for the lossless transmission line is performed by deriving its Z-parameter expressions and then synthesizing these parameters with lumped circuit equivalents.

If the Z-parameters are accurately synthesized, the model will be virtually insensitive to source or load impedances. Two forms of Z-parameter networks are possible: the "T" network and the "I" network. In this report, the "T" network is employed.

#### THE DISTRIBUTED PARAMETER TRANSMISSION LINE (DPTL)

This section describes the necessary equations needed to work with the lossless DPTL. The dominant mode for the propagation of signals is assumed to be transverse electromagnetic (TEM) in which both the electric and magnetic fields are transverse (perpendicular) to the axis of the transmission line. Also, the DPTL is assumed to be uniform and the medium of propagation is

assumed to be homogeneous.

Voltages and currents at any point along the line can be determined if the total voltage and current are known at the sending and receiving ends of that line. Corresponding to Figure 1, we have (1)

$$\begin{array}{c} V_S=V_R \; \cosh \;\; \Upsilon \, \pounds \; + \; I_R Z_0 \; \sinh \;\; \Upsilon \pounds \\ V_R=V_S \; \cosh \;\; \Upsilon \, \pounds \; - \;\; I_S Z_0 \; \sinh \;\; \Upsilon \pounds \end{array} \tag{1}$$
 
$$I_S=I_R \; \cosh \;\; \Upsilon \, \pounds \; + \;\; (V_R/Z_0) \; \sinh \;\; \Upsilon \, \pounds \\ I_R=I_S \; \cosh \;\; \Upsilon \, \pounds \; - \;\; (V_S/Z_0) \; \sinh \;\; \Upsilon \, \pounds \end{array}$$

where,  $Z_0$  = characteristic impedance  $\gamma$  = propagation constant and other quantities are defined in Figure 1.

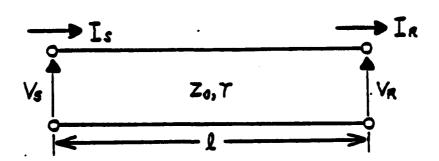


Figure 1

The characteristic impedance and propagation constant are typically expressed as

$$Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}} \qquad Y = \sqrt{(R+j\omega L) (G+j\omega C)}$$
(2)

where, R = resistance per unit length

L = inductance per unit length

G = conductance per unit length

C = capacitance per unit length

If R and G are assumed to be negligible, as for the lossless line, equation (2) becomes

$$Z_0 = \sqrt{\frac{L}{C}}$$
,  $\gamma = jw \sqrt{LC}$   $\triangleq j \in (3)$ 

and substitution into equation (1) yields

$$V_S = V_R \cos 3.2 + jI_R Z_0 \sin 3.2$$
 $V_R = V_S \cos 3.2 - jI_S Z_0 \sin 3.2$ 
 $I_S = I_R \cos \beta.2 + j(V_R/Z_0) \sin 3.2$ 
 $I_R = I_S \cos \beta.2 - j(V_S/Z_0) \sin 3.2$  (4)

The equations in (4) are the only ones required to find the Z parameters of the lossless DPTL.

#### Z-PARAMETERS FOR THE LOSSLESS OPTL

The symmetric and reciprocal DPTL may be fully described by a "T" network incorporating the Z-parameters shown in Figure 2.

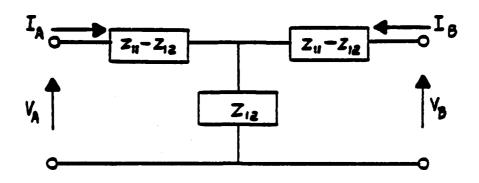


Figure 2

The input and output voltages are determined from

$$V_A = Z_{11} I_A + Z_{12} I_8$$

$$V_B = Z_{21} I_A + Z_{22} I_8$$
 (5)

Since we have symmetry and reciprocity,  $Z_{21} = Z_{12}$  and  $Z_{22} = Z_{11}$  so that (5) becomes

$$V_A = Z_{11} I_A + Z_{12} I_B$$
  
 $V_B = Z_{12} I_A + Z_{11} I_B$  (6)

The equations in (4) may be manipulated so that  $V_S$  and  $V_R$  are in terms of  $I_S$  and  $I_R$ . Upon doing this, we have

$$V_S = -jI_S Z_0 \cot 2\ell + jI_R Z_0 \csc 3\ell$$

$$V_R = -jI_S Z_0 \csc 3\ell + jI_R Z_0 \cot 3\ell \qquad (7)$$

When these equations for  $V_S$  and  $V_R$  are compared to the equations in (6), we can see that we have the relationships between the Z-parameters and the DPTL parameters:

$$Z_{11} = -jZ_0 \cot 3 \ell$$
,  $Z_{12} = -jZ_0 \csc \beta \ell$   
and  $Z_{11} - Z_{12} = jZ_0 \tan 3 \ell / 2$ 

The DPTL may now be represented by the network shown in Figure 3.

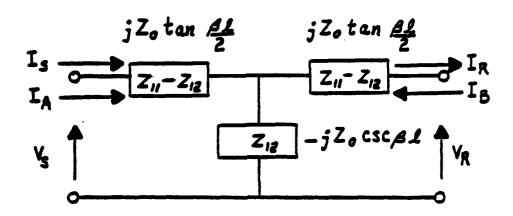


Figure 3

The remaining task is to find circuits which will represent the impedances  $jZ_0$  tan  $\beta \ell$  /2 and  $-jZ_0$  csc  $\beta \ell$  to a high degree of accuracy. The techniques used are discussed in the next section.

#### CIRCUIT SYNTHESIS

The impedances,  $Z_{11}$  - $Z_{12}$  and  $Z_{12}$ , will be synthesized separately. Since these impedances are trigonometric functions, it is suitable to express the sine and cosine in terms of polynomial expansions. (2)

$$\sin x = x (1 + a_2 x^2 + a_4 x^4 + a_6 x^6 + a_8 x^8 + a_{10} x^{10}) + |\epsilon_a|$$
  
 $|\epsilon_a| \le 2x10^{-9}$ ,  $0 \le x \le \pi/2$ 

$$\cos x = 1 + b_2 x^2 + b_4 x^4 + b_6 x^6 + b_8 x^8 + b_{10} x^{10} + |\epsilon_b|$$

$$|\epsilon_b| \le 2x10^{-9}, \ 0 \le x \le \pi/2$$
(8)

csc 
$$X = \frac{1}{X} + 2X \sum_{n=1}^{\infty} \frac{(-1)^n}{X^2 - (n\pi)^2}$$
 (9)

where:

$$a_2 = -.1666666664$$
 $b_2 = -.4999999963$ 
 $a_4 = .0083333315$ 
 $b_4 = .0416666418$ 
 $a_6 = -.0001984090$ 
 $b_6 = -.0013888397$ 
 $a_8 = .0000027526$ 
 $b_8 = .0000247609$ 
 $a_{10} = -.0000000239$ 
 $b_{10} = -.00000002605$ 

Equations in (8) are used for  $jZ_0$  tan  $\beta k$  /2, and equation (9) is used for  $-jZ_0$  csc  $\beta k$ . First, we will synthesize the impedance,  $jZ_0$  tan  $\beta k$  /2, then we will work on  $jZ_0$  csc  $\beta k$ .

SYNTHESIS OF Z11 - Z12

It can be shown that  $\beta \ell / 2 = -jKs$  where  $K = \frac{2\sqrt{\mu \ell}}{2}$  and  $S = j\omega$ . Now we may write  $jZ_0$  tan  $\beta \ell / 2$  as  $jZ_0$  tan (-jKs). Using equations in (8), we get:

$$jZ_{0}tan(-jKs) = jZ_{0} \left[ \frac{-jKs \{1+a_{2}(-jKs)^{2}+a_{4}(-jKs)^{4} + \cdots + a_{10}(-jKs)^{10}\}}{1 + b_{2} (-jKs)^{2} + b_{4} (-jKs)^{4} + \cdots + b_{10} (-jKs)^{10}} \right]$$

$$= Z_{0}Ks - a_{2}Z_{0}K^{3}s^{3} + a_{4}Z_{0}K^{5}s^{5} - a_{6}Z_{0}K^{7}s^{7} + a_{8}Z_{0}K^{9}s^{9} - a_{10}Z_{0}K^{11}s^{11}}{1 - b_{2}K^{2}s^{2} + b_{4}K^{4}s^{4} - b_{6}K^{6}s^{6} + b_{8}K^{8}s^{8} - b_{10}K^{10}s^{10}}$$

$$\frac{\Delta}{a} \frac{N(s)}{D(s)}$$
(10)

Synthetic division of (10) is performed in a manner shown in equation (11) which yields a network of a Cauer form (Figure 4). See Appendix A.

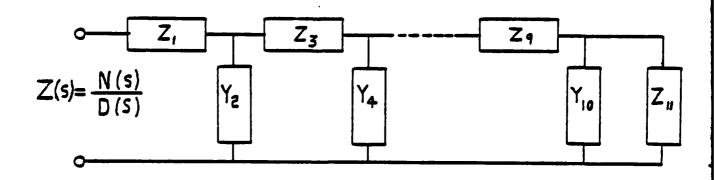
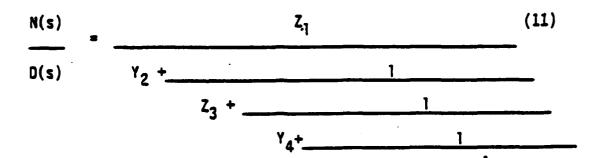


Figure 4



Once the synthetic division is complete, we can find the corresponding circuit elements.

where L is in Henrys and C is in Farads.

Figure 5 shows the completed circuit whose port impedance is  $jZ_0$  tan  $\beta\ell$  /2.

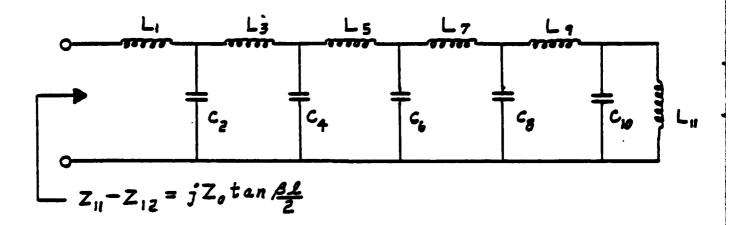


Figure 5

SYNTHESIS OF Z12

For the synthesis of  $Z_{12} = -jZ_0$  csc  $\beta L$ , we use the expansion form of equation (9) but instead of an infinite summation, we will use N terms. Letting  $x = \beta L = -j2Ks$ , we get

$$-jZ_{0} \csc \beta \ell = -jZ_{0} \begin{bmatrix} 1 & +2(-j2Ks) & Z & \frac{(-1)^{n}}{(-j2Ks)^{2}-(n\pi)^{2}} \\ \end{bmatrix}$$

which may be rearranged into

$$-jZ_{0} \csc \beta \ell = Z_{0} + \frac{\Sigma}{n=1} \frac{(-1)^{n} 4Z_{0}Ks}{4K^{2}s^{2} + (n\pi)^{2}}$$
(12)

The addend of equation (12) is of the form as which is a  $bs^2+c$ 

general impedance expression of an LC tank circuit.

Consider the tank circuit of Figure 6; its terminal impedance is given by

$$Z(s) = \frac{sL}{LCs^2+1}$$

which can be forced to equal the addend of (12). By doing this we find that

$$L_n = \frac{(-1)^{-n} 4Z_0 K}{(n\pi)^2}$$
,  $C_n = \frac{K}{(-1)^n Z_0}$ 

The first term of (12) is the impedance of a capacitor whose value is  $2K/Z_0$ . Now the synthesized circuit for  $Z_{12}$  is complete and shown in Figure 7.

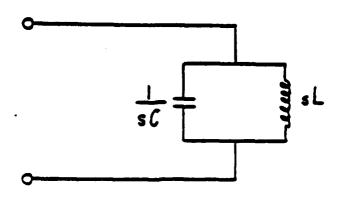


Figure 6

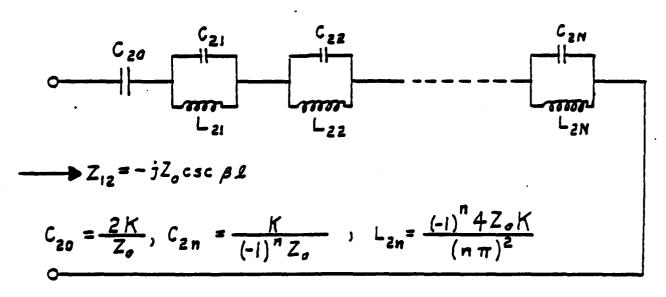


Figure 7

#### THE COMPLETED MODEL AND ITS ANALYSIS

By placing the networks of Figure 5 and Figure 7 into the Z-parameter network of Figure 2, the complete model for the DPTL is developed. Shown in Figure 8 is the model's schematic along with the source and load impedances.

A Fortran Program (Appendix B) has been written in order that the DPTL model may be analyzed for errors in the output voltage. In the program, "MVOD" is the magnitude of  $V_S/V_L$  (See Figure 3) as determined by the use of the standard transmission line equations and "MVOL" is the magnitude of  $V_S/V_L$  as determined by the DPTL model. The error (in dB) (See Figure 9) is defined as

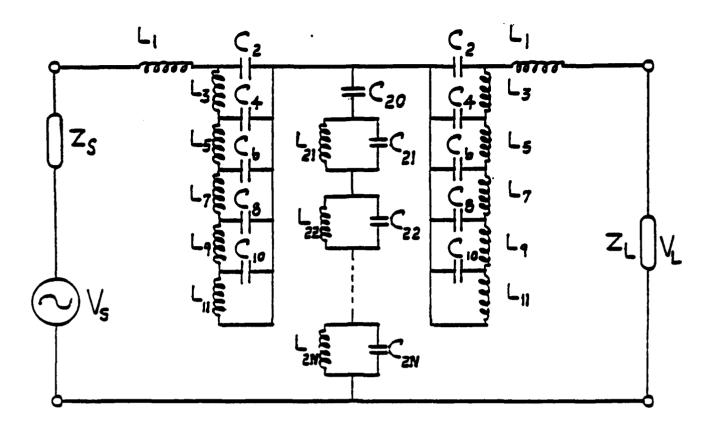
Error dB = 20 Log (MVOL/MVOD)

Resonances along the line are very evident. The errors at  $\lambda/4$  and  $3\lambda/4$  are seen to be small compared to those at  $\lambda/2$  and  $\lambda$ . This is because the approximations of equation (8) are in greatest error at  $x=\pi/2$  and least error at x=0 and  $x=\pi/4$ . The huge error at line lengths of  $\lambda/2$  and  $\lambda$  are not troublesome if one does not include frequencies which correspond to line lengths equal to exactly  $\lambda/2$  and  $\lambda$ .

#### Conclusion and Recommendations

The sample runs in Appendix 8 are for transmission lines with

#### LOSSLESS DETL MODEL



= .04587332KZ

L3 = -01755653KZ

= .03967702KZ

= .38828470KZ

= -11857035KZ₀ = .16229000KZ₀

$$L_{2n} = (-1)^n 2KZ_0$$
 $(n\pi)^2$ 

$$C_2 = .27086265K/Z_0$$

$$C_6 = .12680405 \text{K/Z}_0$$

$$c_{2n} = (-1)^n \frac{\kappa}{2Z_0}$$

Figure 8

 $K = \frac{\beta \ell}{\omega}$ 

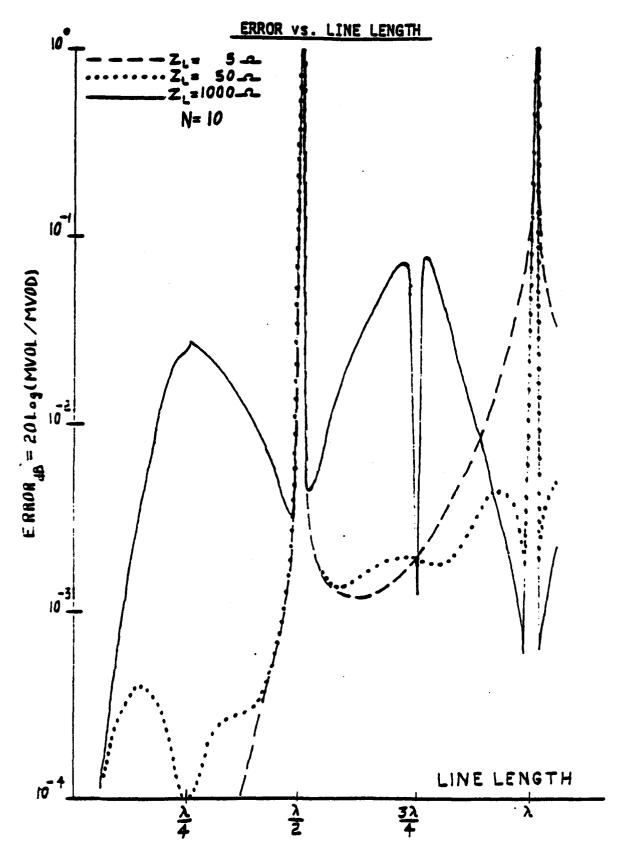


Figure 9

relative permittivity ( $\epsilon_r$ ) equal to one. The program allows one to input other values of  $\epsilon_r$ ; but then, the effective line length will be different.

The errors between calculations from the DPTL model and the transmission line equations are less than one-tenth decibel provided the effective line length is less than or equal to one wavelength. The load,  $Z_L$ , does not significantly affect the results unlike the case of typical lumped circuit models  ${4 \choose 4}$ .

The use of the DPTL model may be found for several applications where line losses are low. When losses are high, this model can no longer be used. Thus, it is recommended that a similar model which considers losses be developed. It is also desirable to test the present DPTL model using nonlinear sources and loads. Once the models for the lossy lines are developed, coupling and cross-talk can be considered next for modeling in terms of lumped circuit components.

#### APPENDIX A

#### The Cauer Network

The synthesis considered here is that for the one-port network. Here, Cauer's method  $^{(3)}$  is used. Cauer networks are derived from the expansion of a rational fraction (equation (A-1)) into the Stieljes' continued fraction expansion (equation (A-2)) which is the same as equation (11).

$$R(s) = \frac{N(s)}{D(s)} = \frac{A_0 s^m + A_1 s^{m-1} + A_2 s^{m+2} + \dots}{B_0 s^n + B_1 s^{n+1} + B_2 s^{n+2} + \dots}$$
(A-1)

Stieljes' continued fraction expansion of (A-1) is

$$R(s) = C_0 s^{m-n} + \frac{1}{C_1 s^{m-n} + \frac{1}{C_2 s^{m-n} + \frac{1}{C_3 s^{m-n} + \frac{1}{1}}}}$$
(A-2)

R(s) has been used to denote either a driving-point impedance, Z(s), or a driving-point admittance, Y(s).

Depending on the values of the A's and B's, some of the capacitances and inductances may have negative values; this should not disturb anyone since the network is not to be realized. Note that if the network is not to be necessarily realizable, we may consider two possible relationships between m and n of equation (A-1).

For equation (10), m = n+1 is used:

$$Z(s) = \frac{A_0 s + A_1 s^2 + A_2 s^3 + \dots + A_{10} s^{11}}{B_0 + B_1 s + B_2 s^2 + \dots + B_{10} s^{10}}$$

which yields the network shown in Figure 4.

#### PROGRAM LISTING

#### LIST TLINE

```
10 COMPLEX Z1, Z2, Z3, Z4, Z5, Z6, Z7, Z8, Z9, Z10, Z11, ZINS, TQ, P
20 COMPLEX ZZI.ZZZ.UU, DNI, DNZ. DN3, DN4, DN5, DN, VOD, ZS, ZL. ZO
25 COMPLEX ZINP.UN.DENI.DEN2.DEN3.DEN4.DEN5.DEN.VOL.T9
30 REAL F.PI.M.LENG.EP.C.FO.FI.F2.LOL
35 REAL Q.QT.T1.T2.T3.T4.T5.T6.FA.SUM
40 REAL BL.BL2.T7.T8.MVOL.MVOD
70 ZO=CMPLX(50..0.)
72 ZS=CMPLX(10.,-25.)
74 ZL=CMPLX(200..500.)
80 P[=3.14159265
90 LENG=1.
110 Er=1.
112 MRITE(6..77) LENG.EH
114 77 FORMAT("LENGHT= ".F12.5.3%,"EPSILJN= ".F12.5)
.116 mRITE(6.76)ZO
.117 ..RITE(6.75)ZS.ZL
118 76 FORMAT("ZO= ".2E12.5)
.119 75 FORMAT("ZS= ".2512.5.3X."ZL= ".2512.5)
120 C=3.E8
122 DO 100 N=10.10000.50
124 F=(FLMAT(N)) *1.56
126 11=2.*[*
130 LOL=LE: 1G * F * SQRT(EP) / (3.25)
140 FO=P[*LOL/+
150 F1=20*F0
100 F2=+0/Z0
170 T=n#F1*.09174664
180 ZI=CMPLX(O..T)
190 T=-1./(n*+2*.5417253)
200 Z2=CAPLX(U..T)
210 T=m*F1*(-.035.1131)
220 Z3=CMPLX(0..T)
230 T=1./(n*F2*.4033141)
240 Z4=CMPLX(0..T)
250 T=n#F1#(.07935403)
260 Z5=CMPLX(0..T)
270 T=-1./(n*F2*.2536081)
280 Z6=CMPLX(0..T)
290 T=##F1*.7765694
300 Z7=CMPLX(0..T)
310 T=1./(n=F2*.05267584)
320 Zb=CMPLX(0.,T)
330 T=-1.*n==1*.2371407
340 Z9=CMPLX(0...[)
350 T=-1./(n*F2*.5359C52)
```

```
360 Z10=CMPLX(0..T)
370 T=#*F1*.32458
380 Z.11=CMPLX(0..T)
390 P=Z9+Z10+Z11/(Z10+Z11)
400 P=Z7+Z8*P/(Z8+P)
410 P=Z5+Z6*P/(Z6+P)
420 'Y=Z3+Z4*P/(Z4+P)
430 ZINS=Z1+Z2*P/(Z2+P)
440 Q=PI*LOL
450 QT=ZO*TAN(Q)
460 TQ=CMPLX(O..QT)
470 TI=4.*EP*LOL*LOL
480 T2=(4./PI)*LOL*SQRT(EP)
485 T3=1./(2.*P[*LDL*SQRT(EP))
467 SUM=0.
488 FA=-1.
490 ⊍0 99 [=1,20
500 T5=(FLOAT(I)) ++2-T!
505 TO= A/TS
MUZ+OT=NUZ CIE
515 FA=-1. *FA
520 99 CONTINUE
> 22 SUM=T3-T2*SUY
525 SUM--1. *ZO*SUM
530 ZINP=CMPLX(O..SUM)
535 UN=ZL*ZINP
540
    JEN 1=ZS+ZL
545 JENZ=ZINS+ZINF
550 JEN3=ZS+ZL
555 DEN4=ZINS*ZIMP*CMPLX(2..0.)
JOO DENS=ZINS*ZINP
565 UEN=UEN 1+DEN2+DEN3+DEN4+DEN5
580 VOL=UN/DEN
562 MVQL=CABS(/QL)
585 dL=LUL*+[*2.
590 aL2=BL/2.
600 T7=TAN(BL2)
605 T8=-1./SIN(3L)
60d T9=CMPLX(0..T8)
610
    ZZ2=T9+Z0
615 ZZ1=ZO+CMPLX(0.,T7)
620 UU=ZL*ZZ2
    JNI=ZS+ZL
625
630
    ON2=ZZ1+ZZ2
635 JN3=Z5*ZL
640 DN4=ZZ (*ZZ2*CMPLX(2...).)
```

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#### Output Samples

RUN TLINE

```
LENGHT=
          1.00000
                  EPSILIN= 1.00000
ZO= 0.50000E 02 0.
   0.10000E 01 0.
                         ZL= 0.10000E 01 0.
FREQ .= 0.10000E 03
                LEN/LAM=
                         0.33333E-01
    0.77473E-02-0.62452E-01
                         VCD= 0.77473E-02-0.62451E-01
MVJL= 0.62930E-01
                MVDD= 0.62930E-01
      0.60000E 08
                 LEN/LAM= 0.20000E 00
VOL= 0.51984E-04-0.91740E-02 VOD= 0.52017E-04-0.91740E-02
:NVIL= 0.91742E-02 MVII= 0.91741E-02
      0.11000E G9
                 LEN/LAM= 0.34467E 00
0.29680E-02
MVCL= 0.29680E-02
                 MVID=
                 LEN/LAX= 0.53333E 00
FREQ. = 0.16000E 09
VCL= -0.96015E-06 0.70077E-03 /DD= -0.96048E-06 0.70069E-03
MVUL= 0.70077E-13
                 MYDU= 0.70069E-03
      0.21000E 09
                 LEN/LAM=
                         0.70000E CO
MVOL= 0.48435E-02
                 MVDD= ).48431E-02
FREQ.= 0.26000E 09
                 LENZLAME 0.86667E 00
    0.30019E-03 0.14969E-01
                         '/ro= 0.29960E-03 0.14964E-01
     0.149725-01
                 MV00= 0.14967E-01
      0.31000E 09
                 LEN/LAM=
                          0.10333E 01
VOL= 0.77U40E-02-0.62281E-01 VOU= 0.77473E-02-0.62451E-01
MVUL= 0.62756E-01 MVUU= 0.62930E-0!
                          0.12000E 01
      0.36000E 09
                 LEH/LAM=
VIL= 0.53130E-04-0.92286E-02 VID= 0.52017E-04-0.91740E-02
                 MVQD= 0.91741E-02
MVDL= 0.92288E-02
  FREQ. = 0.41000E 09
                 LEN/LAH=
                         0.13/67E 01
VGL= -0.11128E-04-0.32494E-02 VDG= -0.11769E-04-0.29680E-02
                 MVDD= 0.29680E-02
MVUL= 0.32494E-02
                 LEN/LAM= 0.15333E 01
      3.460COE 09
0.70069E-03
     0.57938E-03
                 WACD=
```

```
1.000000
LENGHT=
                      EPSILIN=
                                     1.00000
ZO= 0.50000E 02 0.
ZS= 0.10000E 01 0.
                              ZL= 0.50000E 02 0.
                      LEN/LAM=
                                0.3333E-01
       0.10000E 08
VOL= 0.90909E 00-0.29109E 00
                                VDD= 0.90909E 00-0.29109E 00
MVOL= 0.95455E 00
                     MVQD= 0.95455E 00
FREQ. = 0.60000E 08
                      LEN/LA:4=
                                0.20000E 00
VOL= 0.63851E-01-0.44563E 00
                                VOD=
                                      0.63890E-01-0.44567E 00
MVDL= 0.45023E 00
                     MVQD= 0.45022E 00
       0.110COE 09
                      LEN/LAH=
                                0.36467E 00
VCL= -0.14830E-01-0.14656E 00
                                /OU= -0.14815E-01-0.14659E 70
MVJL= 0.14733E 30
                     MV00= 0.14733E 00
rxEQ.= 0.16000E 09
                      LEN/LA4= 0.53333E 70
/OL= -0.12224E-02 0.34991E-0i
                                VOD= -0.12223E-02 0.34987E-01
NVOL= 0.35012E-01
                    MVQD= 0.35 CO85-01
FREQ. = 0.21000E 09
                      LEN/LAM=
                                0.70000E 00
VOL= -0.18133E-01 0.23972E 00
                                VND= -0.13213E-01 0.23969E 10
MVUL= 0.24040E 00
                     MVDD= 0.24038E CO
                                0.34667E 00
        0.260CGE 09
                      LEN/LAM=
VCL= 0.29834E 00 0.58977E 00
                                VOU= 0.298075 00 0.539815 00
MVJL= 0.66094E 20
                     WADD=
                           J.66085E ^0
       0.310CCE 09
                      LEN/LAM=
                                0.103 3E 31
VGL= 0.90867E 00-0.29179E 70
                                VD= 0.30909E 00-0.29109E 00
MVOL= 0.95437E 00
                     MVDD= 0.95455E 00 .
        J.36CCOE 09
                      LEN/LAM=
                                0.12000E 01
      0.55209E-01-0.44801E 00
                                VOU= 0.538905-01-0.44567E 00
MVJL= 0.45273E CC
                     MVDD= 0.45022E 00
raEG. = 0.41000E 09
                      LEN/LAM=
                                0.13667E 01
                                VCD= -0.14815E-01-0.14659E 20
VCL= -0.14016E-01-0.16087E 00
WVDL= 0.16148E 00
                     MVQU= 0.14733E 00
                      LEN/LAM=
                                0.15333E 01
FREQ. = 0.46000E 09
VCL= 0.26747E-02-0.25685E-01
                                VOD= -0.12223E-02 0.34957E-01
```

```
LENGHT=
             1.00000 EPSILEN=
                                     1 _00000
Z0=
    0.50000E 02 0.
ZS=
    0.10000E 01 0.
                               ZL= 0.10000E 04 0.
                   - 20 774E-01
                                0.33333E-01
VOD= 0.10209E 01-0.20.774E-01
                     MYOD= 0.10211E 01
fkEQ.= 0.60000E C5
                      LEN/LAX= 0.20000E 00
      0.27614E 01-0...11435E 01
                                VOD= 0.27602E 01-0.11422E 01
MVDL= 0.29888E 01
                   MVQD= 0.298725 01
                      LEN/LA 4=
FREQ. = 0.11000E 09
                                0.36667E CO
VOL = -0.11695E J1-0.61359E 33 VMD= -0
10 3813E1.. C = = CDVM 10 3702E1.0
                                VDD= -0.117025 01-0.514585 00
AVOL= 0.13207E 01
FREQ. = 0.16000E 09
                      LEH/LAH=
                                0.53333E 10
VQL= -0.32556E CO 0.47613E OO
                                /PD= -0.32555E 00 0.47594E 00
MVJL= 0.57679E 00
                     MVDD= 0.57664E 00
rkEQ.= 0.21000E 09
                      LEN/LAM= 0.70000E 00
VOL= -0.21143E 01 0.15460E 01 VOD= -0.21111E 01 0.15389E 01
10 340262.0 =10VM
                     MVCD= 0.25124E 01
FREQ. = 0.26000E 09
                      LEN/LA := 0.86667E 00
VUL= 0.14702E 01 0.17902E 00
                                VDD= 0.14711E 01 0.17973E 70
                     MVDD= 0.14820E 01
MVOL= 0.148 HE DI
  ens states tenteral a
FREQ. = 0.31000E 09
                      LEN/LAM=
                                0.103338 01
VCL= 0.10210E 01-0.20824E-01
                                VOU= 0.10209E 01-0.20774E-01
AVJL= 0.10212E 01
                     MVD3= 3.102112 31
rkEQ.= 0.36000E 09
                      LEN/LAM=
                                0.12000E 01
/OL= 0.2745dE 01-0...11203E 01
                                VOU= 0.276025 01-0.114225 01
MVDL= 0.29655E 01 MVDU= ().29872E 01
                                0.13667E 01
FREQ. = 0.41000E 09
                      LEH/LA 4=
VUL= -0.13797E 01-0.84378E 00 VND= -0.11702E 01-0.61458E 00
MVOL= 0.16172E 01
                     MV00= 0.13218E 01
FREQ. = 0.46000E 09 LEN/LAM= 0.15333E 01
      0.23431E 00-0.11885E 00 VOD= -0.32553E 00 0.47594E 00
                     MY00= 0.57664E 00
       0.26273E 70
```

```
1.00000
LENGHT=
                     EPSILUN=
                                 1.00000
Z0=
    0.50000E 02 0.
    0.50000E 02 0.
                              ZL= 0.10000E 01 0.
                     LEN/LAM=
                               0.3333E-01
       0_10000E 03
                               VND= 0.181825-01-0.582195-02
VOL= 0.18182E-01-0.58218E-02
                    MVDD= 0.19091E-01
MVDL= 0.19091E-01
                     LEN/LAM= 0.20000E 00
FREQ. = 0.60000E 08
VOL= 0.12770E-02-0.89135E-02
                              VDD= 0.12773E-02-0.89133E-02
                    MVDD= 0.90044E-02
MVDL= 0.900465-02
FREQ. = 0...1000E 09
                     Len/La.4=
                               0.36467E 10
                               VCD= -0.29630E-03-0.29317E-02
VUL= -0.29460E-03-0.29316E-02
MVJL= 0.29466E-02
                    MVDD= 0.29466E-02
                           LEM/LAU=
                               0.53333E 00
FREQ. = 0.16000E 09
                               VOU= -0.24455E-04 0.69974E-03
VCL= -0.24447E-04 0.69961E-03
                    MVQu= 0.70017E-03
      0.70024E-03
#VUL=
                               0.70000E 00
FREQ. = 0.21000E 09
                     LEN/LAH=
                               V∩D= -0.36425E-03 0.47937E-02
VOL= -0.36265E-03 0.47943E-02
MVDL= 0.40080E-02
                    MVD= 0.48075E-02
                     LEN/LAM= - 0.86467E 00
-REQ. = 0.26000E 09
                               VOU= 0.39613E-02 0.11796E-01
VUL= 0.39669E-02 0.11795E-01
       3.13219E-01
                          J.13217E-01
                    M V () U =
                     LEN/LAM=
                               0.10333E 01
rxEQ.= G.31000E G9
                               VOD= 0.18182E-01-0.58219E-02
VCL= 0.18173E-01-0.58358E-02
MYDL= 0.19087E-01
                    MVCD= 0.19091E-01
FREQ. = 0.36000E 09
                     LEN/LA 1=
                               0.12000E 01
                               VOD= 0.12776E-02-0.39133E-02
VCL= 0.13042E-02-0.89603E-02
                    MVDU= 0.90044E-02
4VJL= 0.90547E-02
                               0.13667E 01
FRED. = 0.41000E 09
                      LEN/LAM=
                               VD= -0.29630E-03-0.29317E-02
vuL= -0.25031E-03-0.32173E-02
                    MVQD= J.29466E-02
MVDL= 0.32295E-02
FREQ. = 0.46000E 09
                     LEN/LAM= 0.15333E 01
                               VNU= -0.24455E-04 0.67974E-03
VJL= 0.57493E-04-0.57369E-03
                    M/GD= 0.70017E-03
MVUL= 0.57657E-03
```

```
RUN TLINE
LENGHT=
             1.00000
                      EPSILAN=
                                    1.00000
ZO= 0.50000E 02 0.
                              ZL= 0.50000E 02 0.
0.33333E-01
    0.50000E 02
FREQ.= 0.10000E 08
                     LEN/LAX=
     0.47705E 00-0.12759E 00
                               VOD= 0.47705E 00-0.12759E 00
MVQL=
      0.49381E 00
                    MYOU= 0.49381E 00
       0.40000E 08
                     LEN/LAH=
                               0.20000E 00
     0.60646E-01-0.30743E 00
                               VOD=
                                    0.60692E-01-0.30744E 90
MVDL= 0.31335E 00
                    MVQU=
                           0.31337E 00
 ---
FREQ. = 0.11000E 09
                     LEN/LA:4= 0.36667E 00
VUL= -0.23190E-01-0.12951E 70
                               VOD= -0.23169E-01-0.12952E 10
MVOL= 0.13157E CO
                    MVD= 0.13158E 00
       0.16000E 09
                     Len/Lan=
                               0.53373E 70
VCL= -0.23549E-02 0.34625E-() (
                               VOC= -0.235575-02 0.346215-01
MVJL= 0.34705E-JI
                    10-310745.C =UDVM
FREG. = 0.21000E 09
                               0.70000E 00
                     LEN/LAX=
VOL= -0.23504E-01 0.19404E 00
                               VOD= -0.23598E-01 0.19397E 10
MVOL= 0.19546E 00
                    MVDU= 0.19540E CO
       0.260COE 09
                     LEH/LA 4=
                               0.86467E 30
/UL= 0.21917E OU 0.34005E OU
                               VMD= 7.21894E 00 0.34010E 00
MVUL= 0.40456E 00
                    MYCD= 0.404475 00
        3.3100CE 09
                     LEH/LAM=
                               0.103335 )1
     J.47696E 00-J.12781E 00
                               YQD=
                                    9.47795E 00-0.12759E 10
:AVJL= 0.49379E :00
                    MVQU= 0.49381E 00
       0.36000E 09
                     LENZLA 4= 0.12000E 01
     0.01641E-01-0.30824E 00
                                     0.404925-01-0.307445 70
                               VOD=
MVCL= 0.31435E 00
                    MYOD= 0.31337E 00
       0.41000E 09
                     LEN/LAM= 0.13467E 01
VUL= -0.21639E-01-0.14164E 00
                              VPD= -0.23169E-01-0.12952E 10
      U.14329E 00
                    MVD= 0.13158E 00
       0.46000E 09
                     LEN/LAX=
                               0.15333E 01
/CL= 0.55443E-02-0.25049E-01
                               VOD= -0.23557E-02 0.34621E-01
                     MVQD= 0.347015-01
4VOL= C.28591E-01
```

```
LENGHT=
           1.00000 EPSIL:1N=
                                  1.00000
ZU= 0.50000E 02 0.
ZS= 0.50000E 02 0.
                             ZL= 0.10000E 04 0.
FREQ. = 0.10000E 08
                     LEN/LAM= 0.33333E-01
VOL= 0.92957E 00-0.20245E 00
                             VDD= 0.92957E 00-0.20245E 00
MVOL= 0.95136E 00
                    MVOD= 0.95136E 00
                     LEN/LAM= 0.20000E 00
FREQ.= 0.60000E 08
VOL= 0.26375E 00-0.86246E 00
                             VOD= 0.26402E 00-0.86255E 00
MVDL= 0.90189E 00
                   MVD= 0.90205E 00
                     LEN/LA:4= 0.36667E 00
FREQ. = 0.J1000E 09
VOL= -0.42322E 00-0.65010E 00
                              VOD= -0.42321E 00-0.65058E 00
MVJL= 0.77572E 00
                   MV00= 0.77612E 00
FREQ. = 0.16000E 09
                     LEN/LAM=
                              0.53333E 00
VOL= -0.27546E 00 0.43872E 00
                              VOD= -0.27548E 00 0.43856E 00
MVJL= 0.51802E 00
                    MVQU= 0.51790E CO
FREQ. = 0.21000E 09
                     LEN/LAM=
                              0.70000E 00
VOL= -0.22400E 00 0.80209E 00
                              VDD= -0.22453E 00 0.80098E 00
MYTL= 0.83279E 00 MYTD= 0.83186E 00
FREQ. = 0.26000E 09 LEN/LAM = 0.36667E 00
VOL= 0.6.1185E 00 0.70422E 00
                             VOD= 0.51115E CO 0.70452E CO
MVGL= 0.93289E 00 MVGD= 0.93266E 00
FREQ. = 0.310COE 09
                     LEN/LAM= 0.10333E 01
/QL= 0.9295dE 00-0.20257E 00
                              VDD= 0.32957E 00-0.20245E 00
AVIL 0.95140E 00 MVDD= 0.95136E 00
FREG. = 0.36000E 09
                    LEN/LAM= 0.12000E 01
VUL= 0.26559E 00-0.36048E 00 VND= 0.26402E 00-0.86255E 00
                   MVDD= 0.90205E 00
MVGL= 0.90053E 00
FREQ. = 0.41000E 09
                    LEN/LAM=
                              0.13467E 01
VOL= -0.39161E 00-0.74456E 00 VOD= -0.42321E 00-0.65058E 00
MVQL= 0.84127E 00
                   MVDD= 0.77612E 00
FREQ. = 0.46000E 09
                     LEN/LAM= 0.15333E 01
VUL= 0.23764E 00-0.10132E 00 VDD= -0.27548E 00 0.43856E 00
MVQL= 0.25834E 00 MVQD= 0.51790E 00
```

```
LENGHT=
           1.00000 EPSILON= 1.00000
ZO= 0.50000E 02 0.
    0.10000E 04 0
                    LEN/LAM= 0.33333E-01
FREQ. = 0.10000E 08
VOL= 0.10209E-02-0.20774E-04
                             VOD= 0.10209E-02-0.20.774E-04
MVQL= 0.10211E-02
                   MVOD= 0.10211E-02
                             0.20000E 00
       0.60000E 08
                    LEN/LAX=
VOL= 0.27614E-02-0.11435E-02 VOD= 0.27602E-02-0.11422E-02
MVQL= 0.29888E-02
                   MVQD= 0.29872E-02
FREG. = 0.11000E 09
                   LEN/LAM=
                             0.36667E 00
VOL= -0.11695E-02-0.61359E-03
                             VOD= -0.117025-02-0.61458E-03
MVOL= 0.13207E-02
                   MVOD= 0.13218E-02
       0.16000E 09
                             0.53333E 00
                    LEN/LA:4=
VOL= -0.32556E-03 0.47613E-03
                             VDD= -0.32558E-03 0.47594E-03
                   MYDD= 0.57664E-03
MVUL= 0.57679E-03
       0.21000E 09
                    LEN/LAM= 0.70000E 00
VCL= -0.21143E-02 0.15480E-02 VCD= -0.211.11E-02 0.15389E-02
MVJL= 0.26204E-02 MVDD= 0.26124E-02
FREQ. = 0.26000E 09 LEN/LAM= 10.86667E 00
/QL= 0.14702E-02 0.17902E-03
                             VCD= 0.14711E-02 0.17933E-03
MVOL= 0.148.11E-02 MVOD= 0.14820E-02
       0.31000E 09
                    LEN/LAM=
                             0.103335 01
VGL= 0.10210E-02-0.20824E-04
                            VDD= 0.10209E-02-0.20.7746-04
MVJL= 0.10212E-02
                   MYDD= 0.102.11E-02
FREQ. = 0.36CCOE 09
                    LEN/LAX= 0.12000E 01
     0.2745dE-02-0.11203E-02
                             VDD= 0.27602E-02-0.11422E-02
MVUL= 0.29655E-02 MVUJ= 0.29872E-02
FREG. = 0.41000E 09
                    LEN/LAM= 0.13667E 01
MVOL= 0.16172E-02 MVOD= 0.13218E-02
                    LEN/LAM=
       0.46000E 09
                             0.15333E 01
VOL= 0.23431E-03-0.11885E-03 VDD= -0.32553E-03 0.47594E-03
                   MVOD= 0.57664E-03
MVJL= 0.26273E-03
```

```
LENGHT=
             1.00000
                      EPSILIN=
                                     1.00000
ZO= 0.50000E 02 0.
    0.10000E 04 0.
                               ZL= 0.50000E 02 0.
                               0.3333E-01
FREQ = 0.10000E 08
                     LEN/LAM=
VOL= 0.46478E-01-0.10122E-01
                               VDD= 0.46478E-01-0.10122E-01
                     MVOD= 0.47568E-01
MYUL= 0.47568E-01
                               0.20000E 00
       0.60000E 08
                      LEN/LAH=
     0.13188E-01-0.43123E-01
                               VnD= 0.13201E-01-0.43127E-01
MVOL= 0.45094E-01
                     MVDD= 0.45103E-01
                                0.36667E 00
FREQ. = 0.11000E G9
                      LEN/LAH=
VOL= -0.21161E-01-0.32505E-01
                                VGD= -0.211615-01-0.325296-01
                     MVDU= J.38806E-01
MVQL= 0.38786E-01
FREQ = 0.16000E C9
                                0.53333E 30
                     LEN/LAM=
VOL= -0.13773E-01 0.21936E-01
                               VCD= -0.13774E-01 0.21928E-01
                     MVQU= 0.25895E-01
MVOL= 0.25901E-01
                                0.70000E 00
FREQ. = 0.21000E 09
                      LEM/LAM=
                                VDD= -0.11226E-01 0.40049E-01
VQL= -0.11200E-01 0.40105E-01
MVDL= 0.41639E-01
                     MVDD= 0.41593E-01
                     LEN/LAM= 10.86467E 00
FREQ. = 0.26000E 09
VCL= 0.30593E-01 0.3521:E-01
                                VGD= 0.3055aE-01 0.35224E-01
MVUL= 0.46645E-)1
                     MYDD= 0.46633E-C1
                      LEN/LAM=
                                0.10333E 01
FREQ. = 0.31000E 09
                                VDD= 0.46476E-01-0.10122E-01
VOL= 0.46479E-01-0.10123E-01
                     MVQD= 0.475685-01
MVOL= 0.47570E-01
                                0.12000E 01
                      LEN/LA:4=
FREQ. = 0.36000E 09
                                /CD= 0.13201E-01-0.43127E-01
VOL= 0.13260E-01-0.43024E-01
                     MVDD= 0.45103E-01
MVJL= 0.45027E-01
FREQ. = 0.41000E 09
                      LEN/LAM=
                                0.134678 01
                                VOD= -0.2.11615-01-0.325295-01
VQL= -0.19581E-01-0.37223E-01
MVUL= 0.42063E-01
                     MVQD= 0.38806E-01
                                0.153335 01
        0.46000E 09
                      LEN/LAX=
                                VMD= -0.13774E-01 0.21928E-01
VOL= 0.11382E-01-0.50661E-02
                            3.25395E-01
MVOL= 0.12917E-01
                     WVIIC=
```

#### HUN TLINE

```
LENGHT=
           1.00000
                    EPSILON= 1.00000
ZQ= 0.50000E 02 0.
                           ZL= 0.10000E 04 0.
ZS= 0.10000E 04 0.
                  LEN/LAH= 0.33333E-01
FREQ. = 0.10000E 08
VOL= 0.92062E-01-0.19643E 00
                            VDD= 0.92064E-01-0.19643E 00
MVDL= 0.21693E 00 MVDD= 0.21693E 00
FREQ. = 0.60000E 08
                   LEN/LA4= 0.20000E 00
VOL= 0.16850E-02-0.52204E-01 VOD= 0.16870E-02-0.52219E-01
MVOL= 0.52231E-01
                  MVDD= 0.5.2246E-01
fied.= 0.11000E 09
                   LEN/LAM= 0.36.667E 00
4VUL= 0.65510E-01 AVUU= 0.65537E-01
FREQ. = 0.16000E 09 LEN/LAM = 0.53333E 00
MVDL= 0.16901E CO MVDD= 0.16897E 00
FREQ. = 0.21000E 09
                   LEN/LAM= 0.70000E 00
VQL= -0.16657E-02 0.52007E-01 VQD= -0.16700E-02 0.51955E-01
MVUL= 0.52034E-0! MYGU= 0.51982E-0!
FREQ. = 0.26000E 09 LENZLN4= .0.36667E 00
VGL= 0.39713E-02 0.66510E-01 VCD= 0.3956!E-02 0.46447E-01
MVDL= 0.66.778E-01
                  MVQD= 0.46713E-01
FREQ. = 0.31000E 09
                   LEN/LAM=
                            0.10333E 01
VUL= 0.92009E-01-0.19639E 00 VOU= 0.92064E-01-0.19643E 00
MVUL= 0.21688E 00 MVDD= 3.21693E 00
#EQ.= 0.36000E 09
                  LEN/LAM= 0.12000E 01
VQL= 0.16970E-02-0.32129E-01 VQD= 0.16670E-02-0.5 ?219E-01
MVDL= 0.52157E-01 MVDD= 0.52246E-01
FREQ. = 0.41000E 09 LEN/LA4= 0.13467E 01
VUL= -0.45436E-02-0.65501E-01 VON= -0.57479E-02-0.65284E-01
                  MVDD= 0.65537E-01
MVDL= 0.05658E-01
FREQ.= 0.46000E 09
                   LEN/LAM= 0.15333E 01
VOL= 0:13067E 00 0.46820E-01 VOD= -0.35856E-01 0.15947E 00
MVJL= 0.13880E Q0
                  MVDD= 0.16897E CO:
```

#### REFERENCES

- (1) C.W. Davidson, <u>Transmission Lines for Communications</u>, John Wiley & Sons, New York, 1978, pp. 72-74.
- (2) M. Abramowitz and I.A. Stegun, <u>Handbook of Mathematical</u>
  <u>Functions</u>, Dover Publications, Inc., New York, 1968, pp. 75, 76.
- (3) H.H. Sun, <u>Synthesis of RC Networks</u>, Hayden Book Co., Inc., New York, 1967, pp. 15-22.
- (4) Everett, Woodrow W., III, Department of Electrical Engineering, University of Kentucky, Lexington, Kentucky, "Lumped Model Approximations of Transmission Lines: Effect of Load Impedances on Accuracy," IEEE 1983 International Symposium on Electromagnetic Compatibility, 23-25 Aug 83, Hyatt Regency, Crystal City, Arlington, Virginia.

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## MISSION of Rome Air Development Center

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